11-12 DECEMBER 2011, MIKVE ISRAEL, ISRAEL



# **ACQUIRING KNOWLEDGE OF THE STRUCTURE:** KNOWLEDGE LEVELS, CONFIDENCE FACTORS, TEST METHODS

SPEAKER: PROF. FRANCESCA DA PORTO

DEPARTMENT OF STRUCTURAL & TRANSPORTATIONS ENGINEERING UNIVERSITY OF PADOVA, ITALY





# Safety standards for historical structures

#### <u>Codes</u>

- ISO 13822 bases for design of structures assessment of existing structures (first edition 2001)
- Italian code 'Technical standard for construction' DM 14/01/08 and its explicative documents – (2008)
- EN 1998-3 Eurocode 8 Design of structures for earthquake resistance Part 3 assessment and retrofitting of buildings

#### **Guidelines**

- **Iscarsah** Recommendations for the analysis, conservation, and structural restoration of architectural heritage
- Italian guidelines for the assessment and the reduction of seismic risk of cultural heritage buildings



### MAIN PRINCIPLES FOR EXISTING BUILDINGS (I)

A SUBSTANTIAL PART OF THE NEW ITALIAN SEISMIC CODE IS COMPLETELY DEVOTED TO EXISTING BUILDINGS OF DIFFERENT TYPOLOGIES: R.C. STRUCTURES, STEEL STRUCTURES AND MASONRY BUILDINGS. THE MAIN PRINCIPLES FOR EXISTING BUILDINGS ARE:

1) The degree of uncertainty which affects the safety evaluations of existing buildings and the design of the interventions (... state of the art at the time of construction; non evident effects of conceptual and constructive defects; non evident effects of earthquakes or accidental actions ...) is quantified and taken into account through the use of adequate confidence factors in the safety assessment as well as the use of methods of analysis and assessment that depends on the completeness and reliability of available information

Knowledge level	Confidence factor
LC1	1.35
LC2	1.20
LC3	1.00

2) The difference between UPGRADING (necessary when adding storeys, changing use of the building with consequent increase of loads >20%, substantially changing the building shape and structural behaviour) and IMPROVEMENT (when acting on single structural elements or on monumental buildings), is kept and detailed. *The obligation of safety evaluation for upgrading intervention and the necessity of some kind of evaluation for the improvements is stated*.



# MAIN PRINCIPLES FOR EXISTING BUILDINGS (II)

... AND IN PARTICULAR FOR MASONRY BUILDINGS:

3) The damage on buildings retrofitted after the 1979 earthquake, obtained during the Umbria-Marche earthquake in 1997, underlined the limits of some strengthening techniques which became very popular and even compulsory according to the previous seismic code: they in fact frequently showed scarce performances (injections, jacketing) or even worsened the structural behaviour (jacketing, replacement of flexible floors with stiff floors) of existing masonry buildings.



The execution of interventions that locally change the stiffness of the structure has to be adequately evaluated. The renovation of flexible floors into stiff floors cause a different distribution of seismic actions that can be favourable/unfavourable and has to be taken into account into the modelling and analysis phases.



4) The experience of the Umbria-Marche earthquake, together with experimental and theoretical studies that were carried out, has also underlined some characteristics of the seismic response which are due to the interaction with close buildings or which are due to local effects occurring before a global behaviour can be developed.

For aggregate buildings and mixed structural types, proper structural models have to be chosen. For the evaluation of existing buildings, besides global seismic analyses, local analyses by means of the kinematic mechanisms approach have to be carried out.

**PROF. FRANCESCA DA PORTO** 



#### Italian Standard & Guidelines – Building knowledge

The **knowledge of the masonry historical building**, using particular techniques of analyses and interpretation, is the basis for a reliable appraisal of the seismic safety and for the choice of an effective improvement.

Steps:

Building identification Functional characterisation of the building Geometrical survey Historical analyses of events and past interventions Material and structural survey and conservation state Mechanical characterization of materials Ground and foundations Monitoring









Different knowledge levels and confidence factors CF



#### LEVEL OF KNOWLEDGE & CONFIDENCE FACTORS

TO CALCULATE THE CAPACITY OF THE STRUCTURAL ELEMENTS THE MATERIAL PROPERTIES HAVE TO BE DIVIDED BY THE CONFIDENCE FACTOR, OBTAINED ON THE BASIS OF THE GAINED LEVEL OF KNOWLEDGE

Knowledge level	Geometry	Constructive details	Material properties	Analysis method	Confidence factor FC				
LC1		Limited on-site inspections	Limited on-site testing	All	1.35				
LC2	Structural survey	Extended and	Extended on-site testing	All	1.20				
LC3		comprehensive on- site inspections	Comprehensive on-site testing	All	1.00				
$f_{cd} = f_m / (FC \times \gamma_m)$									
1. GEOMETRY 2. C		ONSTRUCTIVE DETAILS	3. MATERIAL PROPERT		1 C = 1.35)				
		nited on-site inspection	Extended on-site test	↓ LC	2 C = 1.20)				
	co	mprehensive on-site spections	Comprehensive on-site	test 🔶 LC	3 C = 1.00)				

**PROF. FRANCESCA DA PORTO** 



The confidence factor is determined as:

$$F_C = 1 + \sum_{k=1}^4 F_{Ck}$$

Geometrical survey	Material and constructive details inspection	Materials mechanical properties	Ground and foundations
Full geometrical and structural survey $F_{C1} = 0.05$	Limited material and constructive details on site inspection $F_{C2} = 0.12$	mechanical properties obtained from old data $F_{C3} = 0.12$	Limited inspections on ground and foundation, absence of geological data $F_{C4} = 0.06$
Full geometrical and structural survey, with crack and deformation patterns $F_{C1} = 0$	Extended material and constructive details on site inspection $F_{C2} = 0.06$	Limited on site testing on material mechanical properties $F_{C3} = 0.06$	Limited inspections on ground and foundation, presence of geological data $F_{C4} = 0.03$
	Comprehensive material and constructive details on site inspection $F_{C2} = 0$	Extended on site testing on material mechanical properties $F_{C3} = 0$	Extended and comprehensive inspections on ground and foundation $F_{C4} = 0$





# **INFORMATION FOR STRUCTURAL ASSESSMENT**





GEOMETRY, PARTICULAR ELEMENTS (SUCH AS CHIMNEYS, NICHES, ETC), CRACK PATTERN & OUT OF PLUMBS

• by means of surveys

CONNECTIONS, LINTELS, ELEMENTS TO COUNTERACT THRUSTS, VULNERABLE ELEMENTS, MASONRY TIPOLOGY

- limited in situ inspection
- extended & comprehensive *in situ inspection*



MATERIAL PROPERTIES PARTICULARLY AIMED AT THE MECHANICAL CHARACTERIZATION OF MASONRY, THROUGH INSPECTIONS, NDT, MDT & DT

- limited *in situ testing* (inspections)
- extended in situ testing (MDT & NDT)
- comprehensive in situ testing (DT)

#### KNOWLEDGE LEVEL AND CONFIDENCE FACTORS



# **INVESTIGATION PLAN**

#### 1. HYPOTHESYS ON THE BUILDING EVOLUTION

2. IDENTIFICATION OF PLAN-ELEVATION CHARACTERISTICS

3. INTERPRETATION OF CRACK AND DEFORMATION PATTERNS

4. IDENTIFICATION AND CHARACTERIZATION OF CONSTRUCTION DETAILS/ELEMENTS

5. MASONRY TIPOLOGY

6. MATERIALS CHARACTERIZATION

IDENTIFICATION OF RESISTING STRUCTURAL SCHEME, DEFINITION OF ACTIONS AND MECHNICAL PARAMETERS

**PROF. FRANCESCA DA PORTO** 



דו איגוד המהנדסים

# AN EXAMPLE OF HISTORIC SURVEY / BEHAVIOUR









# **1. GEOMETRY**

Geometrical survey includes: survey at each floors of all masonry elements and eventual niches, voids, chimneys, vault survey, floors, roofing, stairs, understaning of loads, foundations.





**PROF. FRANCESCA DA PORTO** 



### 2. CONSTRUCTION DETAILS

a) quality of connections between walls;

b) type and quality of connections between horizontal diaphragms and walls;

- c) type and efficiency of lintels above openings;
- d) presence and efficiency of elements to counteract horizontal trusts;
- e) Presence of structural or non structural elements with high vulnerability;

f) type of masonry





**PROF. FRANCESCA DA PORTO** 

# EXPERIMENTAL INVESTIGATION ON THE BEHAVIOR OF SPANDRELS

IN ANCIENT MASONRY BUILDINGS (Gattesco, Clemente, Macorini, Noè)



Figure 1. Wall with openings sample.



Figure 2. Schematic spandrel loading.



רשות AUTHORITY המהנדסים

DELLI STUDI

IKR







### 2. CONSTRUCTION DETAILS: MASONRY TYPE



**PROF. FRANCESCA DA PORTO** 









וארשות SRAEL AUTHORITY ארשות SRAEL העתיקות העתיקות שום איגוד המהנדסים

IKER

WYORKER

Denti Strad

Santa Gemma, Goriano Sicoli (AQ)



**PROF. FRANCESCA DA PORTO** 



#### 2. CONSTRUCTION DETAILS

This critical analysis is carried out by means of visual inspections, by removing plaster and small masonry dismantling, in order to check both masonry texture and masonry in its thickness, considering also the connections between walls and between walls and floors.





Limited on-site verifications: based on visual surveys, usually through tests on the masonry that lead to superficial examination

**Extended and comprehensive on-site verifications:** based on visual surveys, usually through tests on the masonry that lead to <u>both</u> superficial and deep examination, and of the connection between orthogonal walls.

**PROF. FRANCESCA DA PORTO** 



#### **3. MATERIAL PROPERTIES**

#### Limited on-site investigations:

Information on the material properties, in order to determine the masonry typology. They are based on visual examinations on the masonry surface.

#### Extended on-site investigations:

Tests with double flat jack and characterization tests of the mortar and of stones or bricks. Nondestructive tests (sonic tests, etc...).









#### Comprehensive on-site investigations:

Quantitative information on the material resistance through on-site or laboratory tests (diagonal compression tests on panels or combined tests of vertical compression and shear). Non-destructive tests can be employed in combination, but not in place of the ones above described.

#### USE OF TESTS ON MATERIALS AND STRUCTURES FOR THE EVALUATION OF THE BEARING CAPACITY



בון איגוד המהנדסים

IKR

DELLI STURE

ארשות AUTHORITY



### VALUES OF THE MECHANICAL PROPERTIES (Enc. 11.D)

Table 11.D.1 Reference values of the mechanical parameters (maximum and minimum) and average specific weight for different masonry typologies

	$f_{\rm m}$ (N/cm <sup>2</sup> )	$\tau_0$ (N/cm <sup>2</sup> )	E (N/mm <sup>2</sup> )	G (N/mm <sup>2</sup> )	W (kN/m <sup>3</sup> )	
Tipologia di muratura	min-max	min-max	min-max	min-max	(	
Muratura in pietrame disordinata (ciottoli, pietre erratiche e irregolari)	60 90	2,0 3,2	690 1050	115 175	19	
Muratura a conci sbozzati, con paramento di limitato spessore e nucleo interno	110 155	3,5 5,1	1020 1440	170 240	20	
Muratura in pietre a spacco con buona tessitura	150 200	5,6 7,4	1500 1980	250 330	21	
Muratura a conci di pietra tenera (tufo, calcarenite, ecc.)	80 120	2,8 4,2	900 1260	150 210	16	f <sub>m</sub> = average compression resistance of
Muratura a blocchi lapidei squadrati	300 400	7,8 9,8	2340 2820	390 470	22	the masonry
Muratura in mattoni pieni e malta di calce	180 280	6,0 9,2	1800 2400	300 400	18	$\tau_0$ = average shear resistance of the masonry
Muratura in mattoni semipieni con malta cementizia (es.: doppio UNI)	380 500	24 32	2800 3600	560 720	15	E = average value of the normal
Muratura in blocchi laterizi forati (perc. foratura < 45%)	460 600	30,0 40,0	3400 4400	680 880	12	elasticity modulus
Muratura in blocchi laterizi forati, con giunti verticali a secco (perc. foratura < 45%)	300 400	10,0 13,0	2580 3300	430 550	11	G = average value of the tangential
Muratura in blocchi di calcestruzzo (perc. foratura tra 45% e 65%)	150 200	9,5 12,5	2200 2800	440 560	12	elasticity moutifus
Muratura in blocchi di calcestruzzo semipieni	300 440	18,0 24,0	2700 3500	540 700	14	masonry



### VALUES OF THE MECHANICAL PROPERTIES (Enc. 11.D)

#### Table 11.D.2 Corrective coefficients of the mechanical parameters

Tinologia di muratura	Malta	Ricorsi o	Connessione tracvarcala	Iniezioni di malta	Intonaco
Muratura in pietrame disordinata (ciottoli, pietre erratiche e irregolari)	1,5	1,3	1,5	2	2,5
Muratura a conci sbozzati, con paramento di limitato spessore e nucleo interno	1,4	1,2	1,5	1,7	2
Muratura in pietre a spacco con buona tessitura	1,3	1,1	1,3	1,5	1,5
Muratura a conci di pietra tenera (tufo, calcarenite, ecc.)	1,5	-	1,5	1,7	2
Muratura a blocchi lapidei squadrati	1,2	-	1,2	1,2	1,2
Muratura in mattoni pieni e malta di calce	1,5	-	1,3	1,5	1,5
Muratura in mattoni semipieni con malta cementizia (es.: doppio UNI)	1,3	-	-	-	1,3
Muratura in blocchi laterizi forati (perc. foratura < 45%)	1,3	-	-	-	1,3
Muratura in blocchi laterizi forati, con giunti verticali a secco (perc. foratura < 45%)	1,3	-	-	-	1,3
Muratura in blocchi di calcestruzzo (perc. foratura tra 45% e 65%)	1,3	-	-	-	1,3
Muratura in blocchi di calcestruzzo semipieni	1,3	-	-	-	1,3



#### **MECHANICAL PROPERTIES: USE OF EXPERIMENTAL RESULTS**

- ... THE BELONGING TO AN HIGHER KNOWLEDGE LEVEL INVOLVES ALSO THE POSSIBILITY OF CONSIDERING HIGHER STRENGTH VALUES (IN COMPARISON TO THE PROPOSED RANGES IN TAB. 11.D.1)
- LC1 Resistance and elastic modulus: the minimum of the range
- LC2 Resistance and elastic modulus: the average of the range

LC3 – a) If three experimental values of resistance and elastic modulus are available: average of the experimental values

LC3 – b) If two experimental values of resistance and elastic modulus are available: average of the experimental values, if it is inferior to the upper bound of the table value.

LC3 - c) If one experimental value of resistance and elastic modulus is available: the experimental value is assumed as the value of resistance if it is included in the table range. If not, the average value of the table is assumed.

#### **MECHANICAL PROPERTIES - ENC. 11.D – EXAMPLE** TAB. 11.D.1

	$f_{\rm m}$ (N/cm <sup>2</sup> )	$\tau_0$ (N/cm <sup>2</sup> )	E (N/mm <sup>2</sup> )	G (N/mm <sup>2</sup> )	w (kN/m <sup>3</sup> )	Tipologia di muratura	Malta buona	Ricorsi o listature	Connessione trasversale	Iniezioni di malta
Tipologia di muratura Muratura in pietrame disordinata (ciottoli, pietre erratiche e	min-max	min-max	min-max	min-max		Muratura in pietrame disordinata (ciottoli, pietre erratiche e	1,5	1,3	1,5	2
irregolari)	60 90	2,0 3,2	690 1050	115	19	Muratura a conci sbozzati, con paramento di limitato				
Muratura a conci sbozzati, con paramento di limitato spessore e nucleo interno	110 155	3,5 5,1	1020 1440	170 240	20	spessore e nucleo interno	1,4	1,2	1,5	1,7
Muratura in pietre a spacco con buona tessitura	150	5,6	1500	250	21	Muratura in pietre a spacco con buona tessitura	1,3	1,1	1,3	1,5
Muratura a conci di pietra tenera (tufo, calcarenite, ecc.)	80 120	2,8	900	150	16	Muratura a conci di pietra tenera (tufo, calcarenite, ecc.)	1,5	-	1,5	1,7
Muratura a blocchi lapidei squadrati	300 400	4,2 7,8	2340	390 470	22	Muratura a blocchi lapidei squadrati	1,2	-	1,2	1,2
Muratura in mattoni pieni e malta di calce	180	6,0 9,2	1800	300 400	18	Muratura in mattoni pieni e malta di calce	1,5	-	1,3	1,5
Muratura in mattoni semipieni con malta cementizia (es.: doppio UNI)	380 500	24	2800 3600	560 720	15	Muratura in mattoni semipieni con malta cementizia (es.: doppio UNI)	1,3	-	-	-
Muratura in blocchi laterizi forati (perc. foratura < 45%)	460	30,0 40.0	3400 4400	680 880	12	Muratura in blocchi laterizi forati (perc. foratura < 45%)	1,3	-	-	-
Muratura in blocchi laterizi forati, con giunti verticali a secco (perc. foratura < 45%)	300 400	10,0	2580 3300	430 550	11	Muratura in blocchi laterizi forati, con giunti verticali a secco (perc. foratura < 45%)	1,3	-	-	-
Muratura in blocchi di calcestruzzo (perc. foratura tra 45% e 65%)	150 200	9,5 12,5	2200 2800	440 560	12	Muratura in blocchi di calcestruzzo (perc. foratura tra 45% e 65%)	1,3	-	-	-
Muratura in blocchi di calcestruzzo semipieni	300 440	18,0 24.0	2700 3500	540 700	14	Muratura in blocchi di calcestruzzo semipieni	1,3	-	-	-

Example: masonry in whole bricks and lime mortar:

$$f_{cd}$$
 (LC1) = 180 / (FC = 1.35) x ( $\gamma_m$  = 2) = 67 N/cm<sup>2</sup>

$$f_{cd}$$
 (LC2) = ((180+280)/2) / (FC = 1.20) x ( $\gamma_m$  = 2) = 96 N/cm<sup>2</sup>

 $f_{cd}$  (LC3) = (even superior) ((180+280)/2) / (FC = 1.00) x ( $\gamma_m$  = 2) = 115 N/cm<sup>2</sup>



Intonaco

armato

2.5

2

1.5

2

1,2

1.5

1.3

1.3

1.3

1.3

1.3



presence of transversal connection is

demonstrated:

 $f_{cd (min)} = 180 / (1.35x2) \times 1.5 \times 1.3 = 130 \text{ N/cm}^2$ 



# INVESTIGATION METHODS ON MASONRY BUILDINGS



#### **PROF. FRANCESCA DA PORTO**







**PROF. FRANCESCA DA PORTO** 

# ORIGIN OF THE TABLES 11.D.1 & 11.D.2 (I)

Resistance of the masonry walls: compression



Mechanical properties of the original masonry and after consolidation interventions (E, v, f<sub>m</sub>) through experimental tests









#### ORIGIN OF THE TABLES 11.D.1 & 11.D.2 (II)

#### Resistance of the masonry walls: compression



The compression behavior underlines the differences in terms of resistances and stiffness brought from different kinds of intervention.

**PROF. FRANCESCA DA PORTO** 

.



#### ORIGIN OF THE TABLES 11.D.1 & 11.D.2 (III)

Resistance of the masonry walls: the shear collapse mechanism with diagonal crack is prevalent.



$$f_{\rm t} = \sigma_{\rm t} = \sqrt{\left(\frac{\sigma_{\rm o}}{2}\right)^2 + (b\tau_{H_{\rm max}})^2} - \frac{\sigma_{\rm o}}{2}$$



The shear failure happens when the principal tension stress reaches the limit value  $f_t$ , assumed as the conventional tension resistance of the masonry.

**PROF. FRANCESCA DA PORTO** 



# ORIGIN OF THE TABLES 11.D.1 & 11.D.2 (IV)

Mechanical properties of the original masonry and after the consolidation intervention ( $\tau_0$ , G) through experimental tests



**PROF. FRANCESCA DA PORTO** 



### ORIGIN OF THE TABLES 11.D.1 & 11.D.2 (V)







**PROF. FRANCESCA DA PORTO** 

#### Coring and borehole video-endoscopy:

To understand the morphology of a masonry wall it is important a **direct inspection**. Sometimes it could be performed by removing few bricks or stones. **Coring** should be done with a rotary driller using a diamond cutting edge. A small camera may be inserted into the borehole allowing a detailed study of its surface and try a reconstruction of the wall



Drilled core and reconstruction (Binda, 2000)





**PROF. FRANCESCA DA PORTO** 

#### 

#### Single flat jack test

The determination of the **state of stress** is based on the stress relaxation caused by a cut perpendicular to the wall surface; the stress release is determined by a partial closing of the cutting, i.e. the distance after the cutting is lower than before. A thin **flat-jack** is placed inside the cut and the pressure is gradually increased to obtain the distance measured before the cut.

The equilibrium relationship is the fundamental requirement for all the applications where the flat-jack are currently used (ASTM, 1991):

 $S_f = K_j K_a P_f$ 

 $S_f$  = calculated stress value  $K_j$  = jack calibration constant (<1)  $K_a$  = slot/jack area constant (<1)

 $\mathbf{P}_{f}$  = flat-jack pressure



Single flat-jack test (detection of state of stress) carried out at the Monza Tower (Binda, 1998)



Step 1

**PROF. FRANCESCA DA PORTO** 



#### Double flat jack test

test described can also be The used to determine the deformability characteristics of a masonry. A second cut is made, parallel to the first one and a second jack is inserted, at a distance of about 40 to 50 cm from the other. The jacks delimit a masonry sample of two which a appreciable size to uni-axial compression stress can be applied.



Double flat-jack test (stress-strain behaviour) on West side of the Monza Tower (Binda, 1998)



**PROF. FRANCESCA DA PORTO** 

#### DRILL ENERGY TEST











#### **PULL OUT TEST**






**PROF. FRANCESCA DA PORTO** 

#### Sonic pulse velocity test

The use of sonic tests has the following aims:

- to qualify masonry through the morphology of the wall section;
- to detect the presence of voids and flaws;
- to find crack and damage patterns;
- to control the effectiveness of repair by injection technique.







horizontal vertical





C egg Side 1 2000 2000 1900 1900 1400 1200 1000 m/s

Sonic Tomography

Side 3

# E OF THE STRUCTURE



**PROF. FRANCESCA DA PORTO** 

#### Sonic test

The velocity and waveform of stress waves generated by mechanical impacts can be affected by:

- Input frequency generated by different types of instrumented hammers and transducers;
- Number of mortar joints crossed from the source to the receiver location: the velocity tends to decrease with the number of joints;
- Local and overall influence of cracks.

Local and overall influence of cracks: sonic tests on a pillar of the church of SS. Crocifisso in Noto - SR (Binda, 1999)





**PROF. FRANCESCA DA PORTO** 

Velocità sonica





#### Complementarity of in situ tests

Flat jack tests: some results obtained with single and double flat-jack tests on the external wall of a church, of a bell tower and of a civil building in Campi Alto di Norcia (PG)

Sonic tests: representative diagonal results the of surface sonic measurements on the same walls

**PROF. FRANCESCA DA PORTO** 



#### Thermovision

The **thermographic analysis** is based on the thermal conductivity of a material and may be passive or active. The passive application analyses the radiation of a surface during thermal cycles. If the survey is active, forced heating to the surfaces analyzed are applied

Thermovision can be very useful in diagnostic:

- to identify areas under renderings and plasters,
- to survey cavities,
- to detect inclusions of different materials,
- to detect water and heating systems,
- to detect moisture presence.



Investigation on hidden steel tie rods

**PROF. FRANCESCA DA PORTO** 

Monitoring of the Scrovegni Chapel by IR thermography: Giotto at infrared



FONTE: Grinzato et al., 2002







Dissources Infall Strate at Papers

וארשות SRAEL AUTHORITY ארשות SRAEL העתיקות העתיקות שום איגוד המהנדסים

IKR

**PROF. FRANCESCA DA PORTO** 

#### Georadar

When applied to masonry, the applications of radar procedures can be the following:

- to locate the position of large voids and inclusions of different materials, like steel, wood, etc.;
- to qualify the state of conservation or damage of the walls;
- to define the presence and the level of moisture;
- to detect the morphology of the wall section in multiple leaf masonry.



Radargram of the wall section at the Malpaga Castle





**PROF. FRANCESCA DA PORTO** 





**PROF. FRANCESCA DA PORTO** 





#### **PROF. FRANCESCA DA PORTO**





#### Dynamic tests on ties

 $T{=}(f*\lambda)^2*\mu$ 







Scena f<sub>1</sub>=3.44 Hz

#### **Dynamic identification tests**



1.5E+03

kg/m<sup>3</sup>



ρ

Proprietà

3



ACQUIRING KNOWLEDGE OF THE STRUCTURE

#### **PROF. FRANCESCA DA PORTO**





cracks





Tilting







data-logger



**PROF. FRANCESCA DA PORTO** 

Continue, sciences

ie Matura







דו איאד המהנדסים

IKR

INSTATISTICS. or Paratic

ANTIQUITIES AUTHORITY

#### **PROF. FRANCESCA DA PORTO**





## Example of a monitoring system for the control of the behavior: Qutb Minar – New Delhi (India)

- Positioning of **sensors**:
  - 1 acceleration transducers
  - 2 temperature and R.H. sensor
  - 3 displacement transducer
  - 4 wind velocity and direction transducer
- Data acquisition and analysis



CH1

CH2





**PROF. FRANCESCA DA PORTO** 







רשות AUTHORITY דו איגוד המהנדסים

IKER

WYORKER

DAULT STUDE

**PROF. FRANCESCA DA PORTO** 







#### **PROF. FRANCESCA DA PORTO**



Interno



Università degli Studi di Padova, Facoltà di Ingegneria

Descrizione

PANNELLO 12-13-14-15

#### PANNELLI 12-13-14-15 POST-INIEZIONE

ABRUZZO – INTEGRATION NDT / DT



Esterno





## **ABRUZZO – INTEGRATION NDT / DT**



Sonic pulse velocity before and after grout injections (m/s)

**PROF. FRANCESCA DA PORTO** 







#### **PROF. FRANCESCA DA PORTO**













## L'AQUILA: FORTEZZA SPAGNOLA



esterno in travertino





UNIVERSITA' DI PADOVA	Dipartime Respons	ento di Costruzioni e Trasporti. abile: prof. C. Modena
POLITECNICO DI MILANO	Dipartime Beni Cult	ento di Ingegneria Strutturale – Sezione Murature e surali. Responsabile: prof.ssa L. Binda
ISTITUTO SUPERIORE PER CONSERVAZIONE ED IL RE	LA STAURO	Dr. Roberto Ciabattoni, Dr. Carlo Cacace

Attività di indagine

Monitoraggio strutturale

- □ Identificazione dinamica
- □ Prove soniche per trasparenza
- □ Tomografia sonica
- Termografia attiva
- Prove con martinetti singoli
- Prove con martinetti doppi

- **Controllo dei** parametri ambientali Monitoraggio statico
- Monitoraggio dinamico





UNIVERSITA' DI PADOVA	Dipartime Response	ento di Costruzioni e Trasporti. abile: prof. C. Modena
POLITECNICO DI MILANO	Dipartime Beni Cult	ento di Ingegneria Strutturale – Sezione Murature e Jurali. Responsabile: prof.ssa L. Binda
ISTITUTO SUPERIORE PER CONSERVAZIONE ED IL RE	LA STAURO	Dr. Roberto Ciabattoni, Dr. Carlo Cacace

Attività di indagine

Monitoraggio strutturale

- □ Identificazione dinamica
- Prove soniche per trasparenza
- Tomografia sonica
- Termografia attiva
- Prove con martinetti singoli
- Prove con martinetti doppi

- Controllo dei parametri ambientali
- □ Monitoraggio statico
- Monitoraggio dinamico





UNIVERSITA' DI PADOVA	Dipartime Respons	ento di Costruzioni e Trasporti. abile: prof. C. Modena
POLITECNICO DI MILANO	Dipartime Beni Cult	ento di Ingegneria Strutturale – Sezione Murature e surali. Responsabile: prof.ssa L. Binda
ISTITUTO SUPERIORE PER CONSERVAZIONE ED IL RE	LA STAURO	Dr. Roberto Ciabattoni, Dr. Carlo Cacace

Attività di indagine

Monitoraggio strutturale

- Identificazione dinamica
- Prove soniche per trasparenza
- Tomografia sonica
- Termografia attiva
- Prove con martinetti singoli
- Prove con martinetti doppi

- Controllo dei parametri ambientali
- Monitoraggio statico
- Monitoraggio dinamico





UNIVERSITA' DI PADOVA	Dipartime Response	ento di Costruzioni e Trasporti. abile: prof. C. Modena
POLITECNICO DI MILANO	Dipartime Beni Cult	ento di Ingegneria Strutturale – Sezione Murature e surali. Responsabile: prof.ssa L. Binda
ISTITUTO SUPERIORE PER CONSERVAZIONE ED IL RE	LA STAURO	Dr. Roberto Ciabattoni, Dr. Carlo Cacace

Attività di indagine

Monitoraggio strutturale

dinamico

- □ Identificazione dinamica
- □ Prove soniche per trasparenza
- Tomografia sonica
- Termografia attiva
- Prove con martinetti singoli
- Prove con martinetti doppi

**Controllo dei** parametri ambientali Monitoraggio statico Monitoraggio



UNIVERSITA' DI PADOVA	Dipartime Respons	ento di Costruzioni e Trasporti. abile: prof. C. Modena
POLITECNICO DI MILANO	Dipartime Beni Cult	ento di Ingegneria Strutturale – Sezione Murature e Jurali. Responsabile: prof.ssa L. Binda
ISTITUTO SUPERIORE PER CONSERVAZIONE ED IL RE	LA STAURO	Dr. Roberto Ciabattoni, Dr. Carlo Cacace

Attività di indagine

Monitoraggio strutturale

- □ Identificazione dinamica
- Prove soniche per trasparenza
- □ Tomografia sonica
- Termografia attiva
- Prove con martinetti singoli
- Prove con martinetti doppi

- Controllo dei parametri ambientali
- □ Monitoraggio statico
- □ Monitoraggio dinamico



**PROF. FRANCESCA DA PORTO** 





PROSPETTO SUD-EST

3 4 SETUP 3 3 

Π

5 setup overall 27 acquisition positions.

8 sensors, of which 2 are fixed (X ed Y).

On the internal and external façades.













Another mode emerging from all the measurements is a flexural mode in opposition for the two façades at 5,2 – 5,4 Hz. Other vibration modes are not identified with all set-ups, and are related to the damage and disconnection of the two façades.





**PROF. FRANCESCA DA PORTO** 



















#### **PROF. FRANCESCA DA PORTO**





**PROF. FRANCESCA DA PORTO** 



#### SONIC TESTS



**PROF. FRANCESCA DA PORTO** 



#### SONIC TESTS




**PROF. FRANCESCA DA PORTO** 



SONIC TESTS



**PROF. FRANCESCA DA PORTO** 



SONIC TESTS

**TOMO 2** 







**PROF. FRANCESCA DA PORTO** 



SONIC TESTS



**PROF. FRANCESCA DA PORTO** 





### **PROF. FRANCESCA DA PORTO**



Maggio 2009 rappresentazione delle magnitudo (IGNV) e i rilevamenti dei fessurimetri II giorno 15 maggio Sono stati applicati i tiranti e si giustifica il salto (chiusura della fessura).









Maggio 2009 rappresentazione delle magnitudo (IGNV) e i rilevamenti dei fessurimetri. Il mese è suddiviso due momenti prima dei tiranti. (06-15/05)

**PROF. FRANCESCA DA PORTO** 



MONITORING SYSTEM: DYNAMIC



### **PROF. FRANCESCA DA PORTO**



בן איגוד המהנדסים

IKR

NUMBER

**ENGINEER'S SEMINAR: HISTORIC BUILDINGS AND EARTHQUAKE** 

11-12 DECEMBER 2011, MIKVE ISRAEL, ISRAEL



# THANK YOU!

**SPEAKER: PROF. FRANCESCA DA PORTO** 

DEPARTMENT OF STRUCTURAL & TRANSPORTATIONS ENGINEERING UNIVERSITY OF PADOVA, ITALY

